# High Efficiency LCD Monitor Power Design Using AIC1578 

## DESCRIPTION

The AIC1578 is a high performance step-down DC/DC converter, designed to drive an external P-channel MOSFET to generate programmable output voltages. Two main schematics of Pulse-Skipping and Pulse-Frequency Modulation are employed to maintain low quiescent current and high conversion efficiency under wide ranges of input voltage and loading condition. A current sense comparator with both inverting and non-inverting input uncommitted is included to provide the crucial function of either current limit protection or constant output current control. When the AIC1578 is used in a high-side current source step-down constant current source, the efficiency is typically greater than $90 \%$. Duty cycle can be adjusted to greater than $90 \%$ by connecting a resistor from DUTY pin to VIN. Switching frequency being in around 90 KHZ to 280KHZ range small size switching components
are ideal for portable equipment.

In order to maintain good conversion efficiency form light loads to full loads, the AIC1578 uses the intermittent switch control method of PFM (Pulse-Frequency Modulation) rather than the conventional PWM control method, Fig1. shows its basic structure.

When the feedback voltage is greater than the reference voltage (1.22V),the Err Amp. output is Low, and DRI ( Pin6 ) is Hi Level, turn off outside drive device(P MOSFET), Whereas when the feedback voltage is lower than the reference voltage, the Err Amp is Hi, and DRI( Pin6 ) is Low Level, turn off outside drive device. The kind of control method works similar to PWM at full load, with a stable switch waveform, Whereas when at light load it uses intermittent switching to efficiently sustain output loading requirements.


Fig1. AIC1578 Function Block

In addition, the AIC1578 converter has the following feature:

1. It can operate under an input voltage of 4 V to 20 V.
2. Output voltage can be adjusted externally.
3. It has a PFM design and automatically adjusted switching frequency and duty cycle, which makes it possible to obtain highly efficient conversion over a wide input and output voltage range.
4. It has a shutdown mode control
5. It works in the high frequency range of 90 KHZ to 280 KHZ , and only requires small size
inductors.
6. It has complementary push-pull output, and can drive external P-channel MOSFET or PNP transistor.
7. Low cost.

## Buck Switching Regulator Topology

Basic operation:
Fig. 2 shows the basic structure of an Buck DC/DC converter (switching regulator).



Fig2. Typical Buck Converter Topology

The basic operation principle is to use feedback to control the ON-and-OFF of the power switch to obtain the specified output voltage, for low power applications, conventional PWM control schemes are not ideal, because of, first, the low conversion efficiency due to high switching losses as compared to low output power, and second, the fact that the PWM controller requires a minimum load to maintain its stability. The most efficient and reliable control method is then to use a Pulse-Skipping-Modulation switching control with the control waveforms shown in Fig. 3. This switching control method can put the DC/DC converter into quasi-sleeping mode under no load or light load condition, which reduces switching
losses while maintaining high conversion efficiency and good stability.

In order to choose the appropriate switching converter for an electronic product, therefore, 4 key factors need to be considered:
(1) The current capacity and regulation of the output current should meet what the product demands.
(2) High conversion efficiency.
(3) Low power consumption.
(4) Small size and light weight.


Fig 3. PSM Time Sequence Waveform

## TYPICAL APPLICATION

The circuit shown in Fig. 4 is an output power for LCD MONITOR , when $\mathrm{V}_{\mathrm{IN}}$ is $10 \mathrm{~V} \sim 14 \mathrm{~V}$, a high efficiency of $86 \%$ can be obtained at full load.

| Output Voltage | V OUT | 4.75 | 5 | 5.25 | V |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Output Current | l OUT | 0.2 A |  | 3 A | A |
| Output Ripple <br> Voltage | $\mathrm{V}_{\text {RIPPLE }}$ |  | 100 |  | mV |

(1) Power Specification :

| Item | Symbol | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Input Voltage | $\mathrm{V}_{\mathrm{IN}}$ | 10 |  | 14 | V |



Fig4. AIC1578 for LCD MONITOR Power solution


Fig6. Duty Cycle vs $\mathrm{R}_{\text {DUTY }}$

(ii) Design note and Component selection:

## Design note

1. DC-DC Converter efficiency

Efficiency

$$
=\frac{\text { Pout }}{\text { Pin }}=\frac{\text { lout } \times \text { Vout }}{\operatorname{lin} \times \text { Vin }}=\frac{\text { lout } \times \text { Vout }}{\text { IOUT } \times \text { Vout }+ \text { PLOSS }}
$$

2. Set feedback component ( R1,R2)
following the Datasheet equation :
$V_{\text {OUT }}=1.22\left(1+\frac{\mathrm{R} 1}{\mathrm{R} 2}\right) \Rightarrow \mathrm{R} 1=47 \mathrm{KF}, \mathrm{R} 2=15 \mathrm{KF}$.
(R1+R2) must be bigger than 50KR,for high efficiency request.
C6 is noise filter depend on device's switching frequency.
3. Set Duty range :(if MOSFET CEM4435 : R $\mathrm{R}_{\mathrm{Ds}-\mathrm{on}}$ $=20 \mathrm{mR}, 1 \mathrm{~N} 5820: \mathrm{V}_{\mathrm{F}}=0.475 \mathrm{~V}$ )

D min $=\frac{5+0.475}{14-0.04+0.475}=37.9 \%$
D $\max =\frac{5+0.475}{8-0.04+0.475}=65 \%$
Duty range is : $35.5 \% \sim 65 \%$
See Fig 5 ,When $\mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V} \sim 14 \mathrm{~V}$, $\mathrm{Fsw}_{\text {SW }}$ range is 180 KHZ ~ 230 KHZ and Duty range is $74 \%$ ~ $78 \%$. So, Duty pin can directly connect to VIN pin .If you need larger Duty cycle than typical applications, can reference Fig6 add $\mathrm{R}_{\text {Duty }}$ to adjust it .
4. Set output inductor
$\mathrm{L}=\frac{\left(\mathrm{V}_{\mathrm{DC}}-\mathrm{V}_{0}\right)}{\mathrm{dl}}=\frac{\left(\mathrm{VDC}-\mathrm{V}_{0}\right) \mathrm{ToN}}{0.2 \mathrm{lon}}$

## Component selection :

(1) Sitching MOSFET Selection

The power dissipation of MOSFET is divide into two parts :Conduction losses and Switching losses.
Conduction losses: On-state losses are related to the load current and MOSFET RDS -ON .

$$
P_{C}=I^{2} \text { out } R_{D S-O N} D
$$

Switching losses: These losses are encountered during the MOSFET on and off states. They depend on the nature of the load as well ws the switching speed of the MOSFET.
$P_{S}=f_{S}\left[\int_{0}^{t s 1} V\right.$ Dslddt $+\int_{0}^{\text {ts2 }} V$ Dslodt $]$
$\fallingdotseq \frac{\mathrm{VDSLD}(\mathrm{ts} 1+\mathrm{ts} 2) \mathrm{fs}}{6}$
$\mathrm{f}_{\mathrm{s}}$ : switching frequency
ts1 : turn-on time
ts2 : turn-off time
$\mathrm{V}_{\mathrm{DS}}$ :supply voltage
$I_{D}$ : drain current
Select MOSFET key factors:

1. Low RDS-ON
2. Low CIss
3. Short Reverse recovery time

## (2) SCHOTTKY BARRIER RECTIFIER SELECTION :

 Conduction losses:Diode losses due to recovery time and conduction are strongly related to circuit topology and load impedance.$$
\begin{aligned}
& \mathrm{P}_{\mathrm{CR}}=\mathrm{V}_{\mathrm{F}} \mathrm{l}_{\text {OUT }}(1-\mathrm{D}) \\
& \mathrm{V}_{\mathrm{F}}: \text { Forward Conduction Voltage }
\end{aligned}
$$

Select SCHOTTKY Key factors :

1. Low forward conduction voltage ( $\mathrm{V}_{\mathrm{F}}$ )
2. Low ESR
3. Short Reverse recovery time
4. large Reverse Breakdown Voltage
5. $\mathrm{I}_{\mathrm{D}}-\mathrm{PEAK}>\mathrm{IL}-\mathrm{PEAK}$
(3) PWM Output Capacitors Selection

The bulk filter capacitor values are generally determined by the ESR(effective series resistance) and ESL (effective series inductance) parameters rather than actual capacitance. High frequency decoupling capacitors

Should be placed as close to the power pins of the load as physically possible. Be careful not to add inductance in the circuit board wiring that could cancel the usefulness of these low inductance component, use only specialized low-ESR capacitors intended for switching regulator applications for the bulk capacitors. The bulk capacitor's ESR determines the output ripple voltage and the initial voltage drop after a high slew-rate transient. An aluminum electrolytic capacitor's ESR value is related to the case size
with lower ESR available in larger case sizes.
(4) PWM Output Inductor Selection

The output inductor is selected to meet the output voltage ripple requirements and sets the converter's response time to a load transient. The inductor value determines the converter's ripple current and the ripple voltage is a function of the ripple current. The ripple voltage and current are approximate by the following equation :
$\Delta I=\frac{\text { Vin }^{\prime}-\text { Vout }^{\text {FSLO }}}{\text { Vout }}, ~ \Delta V_{\text {OUT }}=\Delta I \times$ ESR
Increasing the value of inductance reduces the ripple current and converter's response time to a load transient.

## 1. Efficiency Test:

| Input <br> Voltage | Input <br> Current | Output <br> Voltage | Output <br> Current | Output <br> Load | Efficiency |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10 V | 290 mA | 5.06 V | 503 mA | 500 mA | $87.8 \%$ |
| 10 V | 570 mA | 5.06 V | 1003 mA | 1 A | $89.0 \%$ |
| 10 V | 1149 mA | 5.05 V | 2001 mA | 2 A | $87.9 \%$ |
| 10 V | 1754 mA | 5.05 V | 3001 mA | 3 A | $86.4 \%$ |
| 12 V | 252 mA | 5.06 V | 503 mA | 500 mA | $84.2 \%$ |
| 12 V | 489 mA | 5.06 V | 1003 mA | 1 A | $86.5 \%$ |
| 12 V | 979 mA | 5.05 V | 2001 mA | 2 A | $86.1 \%$ |
| 12 V | 1491 mA | 5.06 V | 3001 mA | 3 A | $84.9 \%$ |
| 14 V | 217 mA | 5.09 V | 503 mA | 500 mA | $84.3 \%$ |
| 14 V | 419 mA | 5.09 V | 1003 mA | 1 A | $87.0 \%$ |
| 14 V | 836 mA | 5.08 V | 2001 mA | 2 A | $86.9 \%$ |
| 14 V | 1271 mA | 5.07 V | 3001 mA | 3 A | $85.5 \%$ |

## 2.Temperature Test

| LOAD | LOAD $=1 \mathrm{~A}$ |  |  |  | LOAD = 2A |  |  |  | LOAD $=3 \mathrm{~A}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1578 | MOS | L1 | L2 | 1578 | MOS | L1 | L2 | 1578 | MOS | L1 | L2 |
| 8V | 34.1 | 35.5 | 32.8 | 35.9 | 38.1 | 42.2 | 35.1 | 44.1 | 40.2 | 51.3 | 37.3 | 61.1 |
| 10V | 36.7 | 37.9 | 34.5 | 36.4 | 41.5 | 48.8 | 35.6 | 49.9 | 45.5 | 53.3 | 38.9 | 66.5 |
| 12 V | 39.3 | 38.3 | 34.5 | 36.6 | 43.7 | 51.2 | 36.1 | 50.7 | 49.7 | 65.8 | 37.4 | 70.7 |
| 14V | 40.8 | 40.2 | 34.8 | 37.5 | 44.3 | 56.6 | 38.7 | 62.1 | 50.3 | 66.4 | 39.2 | 74.6 |
| 15V | 42.4 | 40.6 | 35.1 | 39.3 | 45.5 | 58.9 | 39.5 | 69.4 | 53.9 | 67.2 | 44.3 | 80.1 |

Unit: ${ }^{\circ} \mathrm{C}$

## 3.TEST WAVEFORM:

FIG 1: Switching Signal


CH1: VG-GND (5V / DIV)
CH2: VS-GND (5V / DIV)
Status: $\mathrm{V}_{\mathrm{IN}}=10 \mathrm{~V}_{\mathrm{DC}}$
$V_{\text {OUT }}=5.06 \mathrm{~V}_{\text {DC }}$
Output Load $=1 \mathrm{~A}$

FIG 2: Switching Signal


CH1: VG-GND (5V / DIV)
CH2: VS-GND (5V / DIV)
Status: VIN $=12 V_{D C}$

$$
V_{\text {OUT }}=5.05 \mathrm{~V}_{\mathrm{DC}}
$$

Output Load $=2 \mathrm{~A}$

FIG3: Switching Signal


$$
\begin{array}{ll}
\text { CH1: VG-GND }(5 \mathrm{~V} / \mathrm{DIV}) \\
\text { CH2: VS-GND }(5 \mathrm{~V} / \mathrm{DIV}) \\
\text { STATUS: } & \text { VIN= } 10 \mathrm{Vdc} \\
& \text { VOUT }=5.05 \mathrm{Vdc} \\
& \text { Output Load }=3 \mathrm{~A}
\end{array}
$$

FIG5: Switching Signal


CH1: VG-GND (5V / DIV)
CH2: VS-GND (5V / DIV)
Status: $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}_{\mathrm{DC}}$
$\mathrm{V}_{\text {OUT }}=5.05 \mathrm{Vdc}$
Output Load $=2 \mathrm{~A}$

FIG4: Switching Signal


FIG 6: Switching Signal


CH1: VG-GND (5V / DIV)
CH2: VS-GND (5V / DIV)
Status: $V_{I N}=12 V_{D C}$
$\mathrm{V}_{\text {OUT }}=5.06 \mathrm{Vdc}$
Output Load $=3 \mathrm{~A}$

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FIG7: 5V output ripple voltage


CH1: 5V Output (Ripple Voltage)
Status: Input Voltage: 10V
Output Load: 1A

FIG 9: 5V output ripple


CH1:5V Output (Ripple Voltage)
Status: Input Voltage: 12V
Output Load: 1A

FIG 8: Switching Signal


CH1: 5V Output (Ripple Voltage)
Status: Input Voltage: 10V
Output Load: 3A

FIG 10: 5V output ripple


CH1: 5V Output (Ripple Voltage)
Status: Input Voltage: 12V
Output Load: 3A

## 4. LCD MONITOR BOM LIST

| Reference | Part Number | QTY | PKG | Manufacturer | Remark |
| :--- | :--- | :---: | :--- | :--- | :--- |
| Q1 | AIC1578CS | 1 | SO-8 | AIC |  |
| Q2 | CEM4435 | 1 | SO-8 | CET | N-MOSFET |
| Q3 | AIC1085CM | 1 | TO-263 | AIC |  |
| L1 | $1 \mu \mathrm{H} / 2 \mathrm{~A}$ | 1 | SMD | H\&D / Cailcraft |  |
| L2 | $47 \mu \mathrm{H} / 3 \mathrm{~A}$ | 1 | SMD | H\&D / Cailcraft |  |
| D1 | 1 N 5820 | 1 | DIP |  | Schottky |
| C1,C2,C3,C4 | $470 \mu \mathrm{~F} / 16 \mathrm{~V}$ | 4 | DIP |  |  |
| C5 | $220 \mu \mathrm{~F} / 16 \mathrm{~V}$ | 1 | DIP |  |  |
| C6 | 330 PF | 1 | SMD |  |  |
| C7,C8 | $10 \mu \mathrm{~F} / 16 \mathrm{~V}$ | 2 | DIP |  |  |
| C9,10 | $0.1 \mu \mathrm{~F}$ | 2 | SMD |  |  |
| C11 | $0.01 \mu \mathrm{~F}$ | 1 | SMD |  |  |
| R1 | $47 \mathrm{~K} \Omega / 1 \%$ | 1 | SMD |  |  |
| R2 | $15 \mathrm{~K} \Omega / 1 \%$ | 1 | SMD |  |  |
| R3 | $12 \mathrm{~K} \Omega / 1 \%$ | 1 | SMD |  |  |
| R4 | $750 \Omega / 1 \%$ | 1 | SMD |  |  |

